MS181 Phase-field and gradient damage models for fracture in complex materials

Phase-Field Fatigue Modeling in Ductile Materials

Vladimir Dunić, Miroslav Zivkovic, Vladimir Milovanovic

Faculty of Engineering, University of Kragujevac, Serbia

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Outline

1. Introduction
2. Phase-field damage model
3. Fatigue degradation function
4. Example
5. Conclusions

- Low cycle fatigue (LCF) is repeated loading-unloading of material that exhibits plastic strains.
- The loading amplitude is above the yield strength.
- Von Mises plasticity and Phase-field Damage model can be used to create multifield finite elements to compute damage as additional degree of freedom.
- In this work, we compared the simulation results of damage in metals by PFDM implementation by two implementations:
  - Work-densities-based criterion with threshold [Miehe et al.][1]
  - Work-densities-based criterion without threshold[1] in combination with Ambati et al.[2] coupling to plasticity and modifications in Zivkovic et al.[3]
- The fatigue degradation function [Simoes et al.][4] is implemented for simulating accumulation of damage in the material.

[1] Miehe C., Hofacker M., Schanzel L.-M., Aldakheel F. (2015) Phase field modeling of fracture in multi-physics problems. Part II. Coupled brittle-to-ductile failure criteria and crack propagation in thermo-elastic–plastic solids, CMAME, 294, 486-522

[2] Ambati, M., Gerasimov, T., De Lorenzis, L. (2015) Phase-field modeling of ductile fracture. Comput Mech 55, 1017–1040

[3] Zivkovic, J., Dunic, V., Milovanovic, V., Pavlovic, A., Zivkovic (2021) M. A Modified Phase-Field Damage Model for Metal Plasticity at Finite Strains: Numerical Development and Experimental Validation, Metals, 11, 47

[4] Simoes, M, Braithwaite, C, Makaya, A, Martínez-Pañeda, E. (2022) Modelling fatigue crack growth in shape

Phase-field damage model

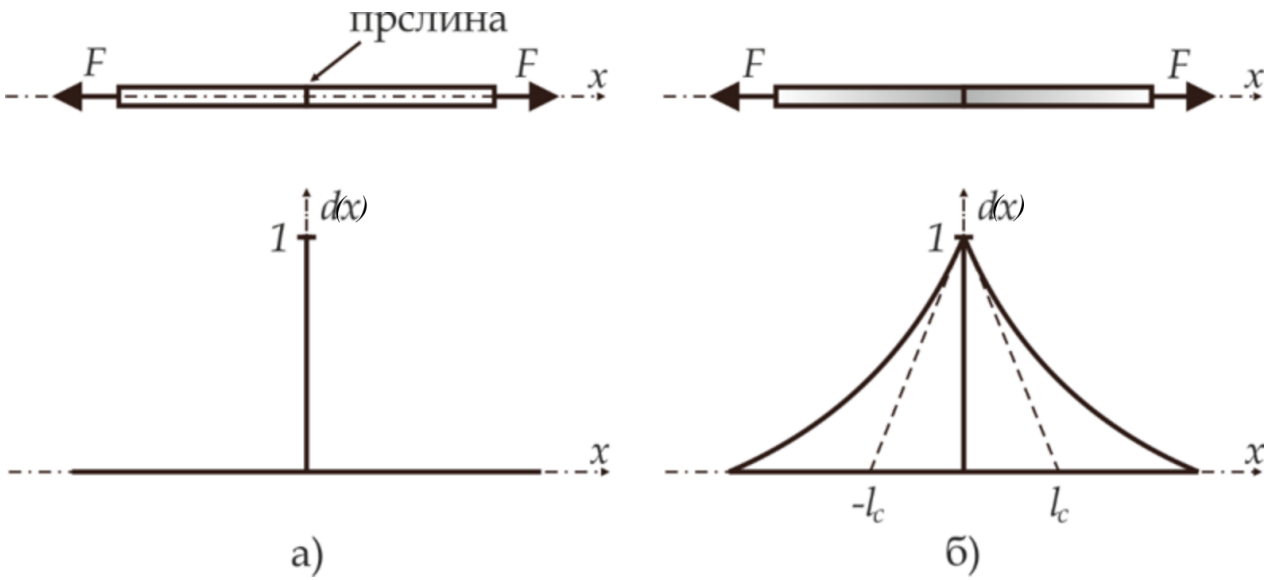


Figure: Crack topology a) discrete and b) diffusive

Phase-field damage variable:

$$d(x) = \begin{cases} 1 & x = 0 \\ 0 & x \neq 0 \end{cases} \qquad d(x) = e^{-\frac{|x|}{l_c}} \tag{1}$$

l_c is the characteristic length (crack width).

The internal potential energy density ψ is considered as the sum of elastic $\psi^E(\boldsymbol{\varepsilon}_E, d)$, plastic $\psi^P(\bar{\varepsilon}_P, d)$, and fracture contribution $\psi^{frac}(d, \nabla d)$ energy density:

$$\psi = \psi^E(\boldsymbol{\varepsilon}_E, d) + \psi^P(\bar{\varepsilon}_P, d) + \psi^{frac}(d, \nabla d) \tag{2}$$

The total internal potential energy W_{int} functional is defined according to Ambati et al. and Zivkovic et al. as

Case 1

$$W_{int} = \int_V \psi dV = \int_V \{g(d)\,\psi^E(\boldsymbol{\varepsilon}_E, d) + \psi^P(\bar{\varepsilon}_P, d) + G_V\left[\frac{d^2}{2} + \frac{l_c^2}{2}|\nabla d|^2\right]\} dV$$

while according to Miehe et al. it is:

Case 2

$$W_{int} = \int_V \psi dV = \int_V \{g(d)\left(\psi^E(\boldsymbol{\varepsilon}_E, d) + \psi^P(\bar{\varepsilon}_P, d)\right) + G_V\left[d + \frac{l_c^2}{2}|\nabla d|^2\right]\} dV$$

where a critical fracture energy release rate per unit volume is $G_V = \frac{G_c}{l_c}$.

The equilibrium of the internal and external potential energy

$$\delta W_{int} = \delta W_{ext} \tag{3}$$

leads to the equilibrium equation:

$$Div\left[\boldsymbol{\sigma}\right] + \mathbf{b} = 0 \tag{4}$$

plasticity yield condition law:

$$\bar{\sigma}_{eq} - \sigma_{yv} - \left(\sigma_{y0,\infty} - \sigma_{yv}\right)\left(1 - e^{-n\bar{\varepsilon}_P}\right) - H\bar{\varepsilon}_P = 0 \tag{5}$$

and the phase field damage evolution law according to Ambati et al. and Zivkovic et al.: Case 1

$$G_V\left[d - l_c^2\nabla^2 d\right] + g'\left(d\right) max\left(\psi^E\right) = 0 \tag{6}$$

and according to to Miehe et al.: Case 2

$$G_V\left[d - l_c^2\nabla^2 d\right] + g'\left(d\right) max\left(\psi^E + \psi^P - \frac{G_v}{2}\right) = 0 \tag{7}$$

Critical total strain vs fracture energy

NOT AVAILABLE AT THE MOMENT

Figure: Fracture energy value and critical total strain

Degradation function for plasticity

Degradation function for Case 1:

$$g(d) = (1-d)^{2p} \tag{8}$$

In Zivkovic et al.[3], the modified damage-plasticity coupling variable is introduced as:

$$p = \begin{cases} 0 & ; \frac{\overline{\varepsilon}_p}{\overline{\varepsilon}_p^{crit}} < 1 \\ \frac{\overline{\varepsilon}_p}{\overline{\varepsilon}_p^{crit}} - 1 & ; \frac{\overline{\varepsilon}_p}{\overline{\varepsilon}_p^{crit}} \geq 1 \end{cases} \tag{9}$$

Degradation function for Case 2:

$$g(d) = (1-d)^{2} \tag{10}$$

[2] Ambati, M., Gerasimov, T. De Lorenzis, L. Phase-field modeling of ductile fracture. Comput Mech 55, 1017–1040 (2015).

[3] Zivkovic, J., Dunic, V., Milovanovic, V., Pavlovic, A., Zivkovic, M. (2021) A Modified Phase-Field Damage Model for Metal Plasticity at Finite Strains: Numerical Development and Experimental Validation. Metals, 11(1), 47

Fatigue degradation function

The field equation corresponding to phase field variable is given as[5]:

$$f\left(\bar{\alpha}(t)\right) G_V(\xi)\left[d - l_c^2 \nabla^2 d\right] + g'(d)\,\psi = 0 \tag{11}$$

where $\bar{\alpha}(t)$ is cumulation of any scalar quantity which can describe the fatigue history experienced by the material. For a pseudo-time τ, the cumulative history variable can be defined as:

$$\bar{\alpha}(t) = \int_0^t H(\alpha\dot{\alpha})|\dot{\alpha}|d\tau \tag{12}$$

where $H(\alpha\dot{\alpha})$ is the Heaviside step function, defined as $H(\alpha\dot{\alpha}) = 1$ if $\alpha\dot{\alpha} \geq 0$ (loading) and $H(\alpha\dot{\alpha}) = 0$ otherwise (unloading).

[5] Simoes, M, Braithwaite, C, Makaya, A, Martínez-Pañeda, E. Modelling fatigue crack growth in shape memory alloys. Fatigue Fract Eng Mater Struct. 2022; 45(4): 1243-1257

- $\bar{\alpha}$ only grows during loading.
- $\alpha = g(d)\psi$ is the fatigue history variable represents the loading conditions in the solid
- $f(\bar{\alpha}(t))$ is the fatigue degradation function characterizes the sensitivity of the fracture energy to the number of cycles.

$$f(\bar{\alpha}(t)) = \begin{cases} 1 & \text{if} \quad \bar{\alpha} \leq \alpha_T \\ \left(\frac{2\alpha_T}{\bar{\alpha}(t)+\alpha_T}\right)^2 & \text{if} \quad \bar{\alpha} > \alpha_T \end{cases} \tag{13}$$

- α_T represents a threshold value, below which the fracture energy remains unaffected:
  Simoes et al. Case 1

$$\alpha_T = \frac{G_V}{12} \tag{14}$$

  Miehe et al. Case 2

$$\alpha_T = \frac{G_V}{2} \tag{15}$$

Uniaxial loading of unit cube

The unit cube is loaded by prescribed displacement on one side, while the other side is restrained.

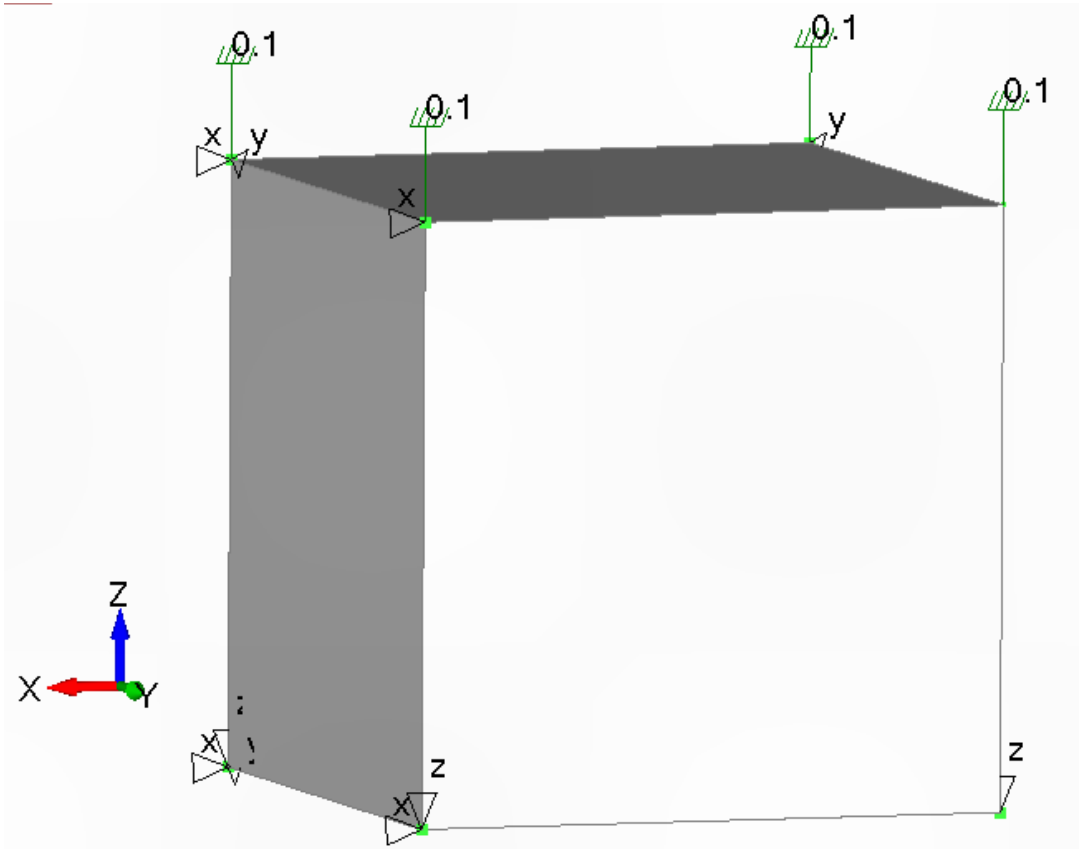


Figure: Boundary and loading conditions of uniaxial loading example

Table: Elasto-plasticity material parameters

E	ν	n
199000 MPa	0.29	18 MPa
σ_{y0}	$\sigma_{y\infty}$	H
345 MPa	635 MPa	9 MPa [-]

Table: Phase-Field damage model parameters

	G_v	$\overline{e}_p^{crit}$	$\overline{e}^{crit}$	l_c
Case 1	2.5 MPa	0.009		0.1 mm
Case 2	82.2 MPa		0.012	0.1 mm

Three loading-unloading cycles are performed up to strain: the first cycle = 2%, the second cycle = 3%, the third cycle 4%.

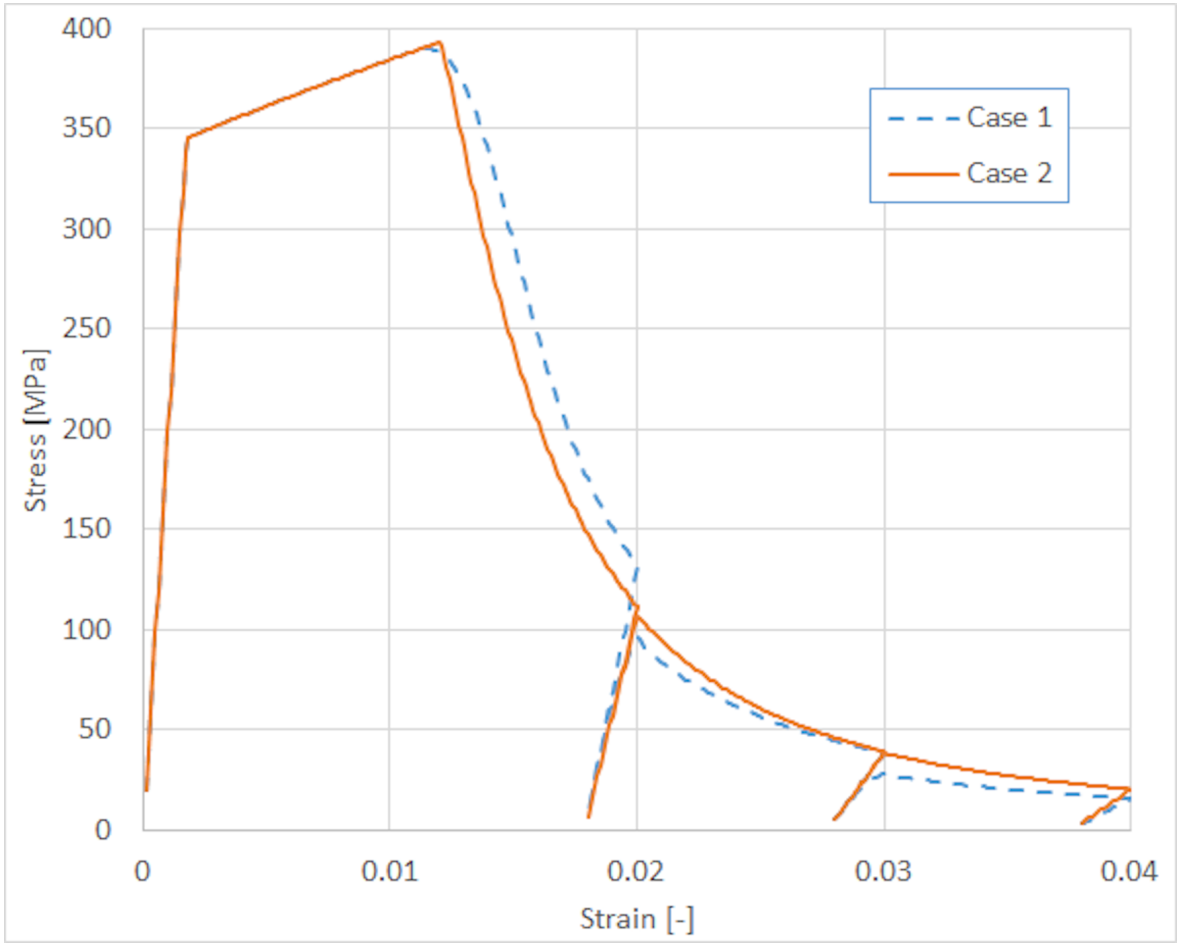


Figure: Stress-strain response

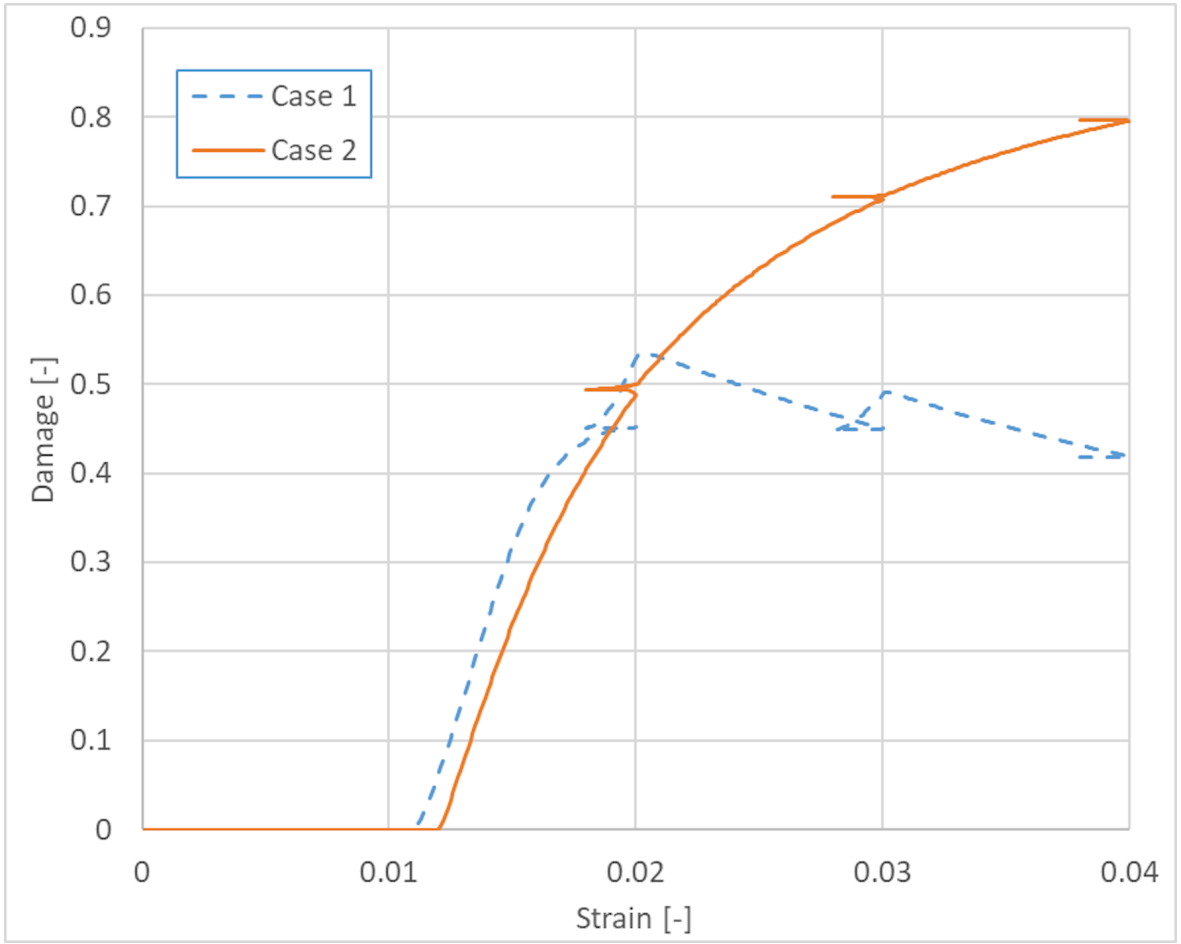
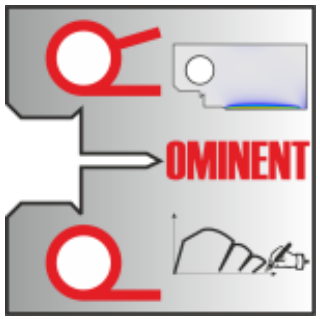


Figure: Damage-strain response

Conclusions

- PFDM is often implemented into FEM for computation of damage and fracture in structures
- The fatigue degradation function opens the possibility to simulate accumulation of damage and fatigue
- Von Mises plasticity constitutive model with Simo hardening function with PFDM and fatigue degradation function is used to show influence of cyclic loading to ductile behavior of metals
- Simple unit cube model is used to show phenomenology and implementation.
- The behavior is shown by stress-strain and damage strain relationships.
- Two implementations are compared and Case 2 offers better control over simulation of damage in ductile materials in fatigue conditions.



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- development of FEM software PAK-DAM for the simulation of damage initiation, evolution and propagation to the fracture,
- experimental investigation of the materials (steel, aluminum, concrete),
- testing and verification of the software functionality and accuracy,
- budget cca 284.000e in period 2024-2026
- https://prominent.kg.ac.rs/